**Community Services Department** 

# Planning and Building

## SPECIAL USE PERMIT (see page 7)

## SPECIAL USE PERMIT FOR GRADING (see page 9)

# **APPLICATION**



Community Services Department Planning and Building 1001 E. Ninth St., Bldg. A Reno, NV 89512-2845

Telephone: 775.328.6100

## Washoe County Development Application

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Building staff at 775.328.6100.

Project Information Staff Assigned Case No.:				
Project Name: Gail Willey Landscaping crop production of trees				
Project Description: landscape business				
Project Address: 190 US Hwy 3	95 South			
Project Area (acres or square fe	et): 3.76 acres			
Project Location (with point of re	eference to major cross	streets AND area locator):		
US 395 South, 0.78 mile	s south of Eastla	ke Blvd on the southeast	side of US 395	
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No.(s):	Parcel Acreage:	
050-220-37	3.76			
Indicate any previous Wash	oe County approval	s associated with this applica	tion:	
Case No.(s).				
Applicant In	formation (attach	additional sheets if neces	sary)	
Property Owner:		Professional Consultant:		
Name: Gail Willey Landscaping		Name: Reno Tahoe Geo Associates, Inc.		
Address: 490 US Highway 395 South		Address: 12000 Old Virginia Road		
Reno, Nevada Zip: 89704		Reno, Nevada Zip: 89511		
Phone: (775) 691-5297 Fax:		Phone: (775) 853-9100 Fax:		
Email: john@gailwilley.com/suzanne@gailwilley.com		Email: ccarnes@rtgeo.com		
Cell: Other:		Cell: (775) 741-2300	Other:	
Contact Person: John Willey		Contact Person: Chad E. Carnes, P.E.		
Applicant/Developer:		Other Persons to be Contacted:		
Name: SAME AS OWNER		Name: Reno Tahoe Geo Associates, Inc.		
Address:		Address: 12000 Old Virginia Road		
	Zip:	Reno, Nevada	Zip: 89511	
Phone:	Fax:	Phone: (775) 853-9100 Fax:		
Email:		Email: ziler@rtgeo.com		
Cell: Other:		Cell: (775) 391-6148 Other:		
Contact Person:		Contact Person: Zach Iler		
	For Office	Use Only		
Date Received:	Initial:	Planning Area:		
County Commission District:		Master Plan Designation(s):		
CAB(s):		Regulatory Zoning(s):		

## Special Use Permit Application Supplemental Information

(All required information may be separately attached)

1. What is the project being requested?

Grading and placement of loose fill material on a parcel intended for crop production of specemin trees for landscape business.

2. Provide a site plan with all existing and proposed structures (e.g. new structures, roadway improvements, utilities, sanitation, water supply, drainage, parking, signs, etc.)

Civil improvement sheet C1.0 is attached with grading and drainage

3. What is the intended phasing schedule for the construction and completion of the project?

Install temporary BMP's, clearing, landscape fill placement, restore temporary BMP's to post construction condition.

4. What physical characteristics of your location and/or premises are especially suited to deal with the impacts and the intensity of your proposed use?

Ease of access to the site from the highway, natural drainage paths, site shape and orientation, benefit to neighboring properties.

5. What are the anticipated beneficial aspects or affects your project will have on adjacent properties and the community?

The planted trees and graded parcel will provide the Old Washoe Estates community with improved privacy, noise reduction, and aesthetic value. The project will also provide the community with trees for landscaping purposes.

6. What are the anticipated negative impacts or affect your project will have on adjacent properties? How will you mitigate these impacts?

None. On-site drainage will be changed from sheet flow across the site to low point where it ponds until it reaches the overflow in the natural drainage to directed flow in drainage swales intermittent with detention basins along edges of the property to mimic the natural detention time.

7. Provide specific information on landscaping, parking, type of signs and lighting, and all other code requirements pertinent to the type of use being purposed. Show and indicate these requirements on submitted drawings with the application.

Landscaping to be added throughout the project and continued into post project timelines.

8. Are there any restrictive covenants, recorded conditions, or deed restrictions (CC&Rs) that apply to the area subject to the special use permit request? (If so, please attach a copy.)

🗆 Yes	D No	

9. Utilities:

a. Sewer Service	Provided by engineered on-site disposal system
b. Electrical Service	NV energy
c. Telephone Service	
d. LPG or Natural Gas Service	
e. Solid Waste Disposal Service	none
f. Cable Television Service	
g. Water Service	proposed well

For most uses, Washoe County Code, Chapter 110, Article 422, Water and Sewer Resource Requirements, requires the dedication of water rights to Washoe County. Please indicate the type and quantity of water rights you have available should dedication be required.

h. Permit #	N/A	acre-feet per year
i. Certificate #	N/A	acre-feet per year
j. Surface Claim #	N/A	acre-feet per year
k. Other #	N/A	acre-feet per year

Title of those rights (as filed with the State Engineer in the Division of Water Resources of the Department of Conservation and Natural Resources).

# N/A

#### 10. Community Services (provided and nearest facility):

a. Fire Station	Truckee Meadows Fire Station 32
b. Health Care Facility	Renown Health (North), Carson Tahoe Regional Medical Center (South)
c. Elementary School	Pleasant Valley Elementary School
d. Middle School	Marce Herz Middle School
e. High School	Damonte Ranch High School
f. Parks	Pleasant Valley Park
g. Library	South Valleys Library
h. Citifare Bus Stop	Herze Boulevard and Mt. Rose Highway

### Special Use Permit Application for Grading Supplemental Information

(All required information may be separately attached)

1. What is the purpose of the grading?

Provide drainage for the site and proper tree planting.

2. How many cubic yards of material are you proposing to excavate on site?

Landscaping to be added throughout the project and continued into post project timelines.

3. How many square feet of surface of the property are you disturbing?

163,785 sq. ft.

4. How many cubic yards of material are you exporting or importing? If none, how are you managing to balance the work on-site?

Approximately 13,000 cubic yards of loose landscape fill will be imported.

5. Is it possible to develop your property without surpassing the grading thresholds requiring a Special Use Permit? (Explain fully your answer.)

It is not possible as the middle portion of the site needs to be raised so water can drain to the existing natural drainage path without causing damage to the proposed access road and parking lot.

6. Has any portion of the grading shown on the plan been done previously? (If yes, explain the circumstances, the year the work was done, and who completed the work.)

No, the grading work has not been started.

7. Have you shown all areas on your site plan that are proposed to be disturbed by grading? (If no, explain your answer.)

Yes, all areas of disturbance by grading have been shown on Plan Sheet C1.0.

8. Can the disturbed area be seen from off-site? If yes, from which directions and which properties or roadways?

Yes, the disturbed area can be seen from US Hwy 395 South and Old Washoe Drive however, the property is proposed to be screened from view by large trees. The disturbed areas can been seen from properties 144 Old Washoe Drive, 150 Old Washoe Drive and 220 US Hwy 395 South. Some areas are currently planted with trees and screen the property from the neighboring parcels.

9. Could neighboring properties also be served by the proposed access/grading requested (i.e. if you are creating a driveway, would it be used for access to additional neighboring properties)?

No access needed for neighboring properties as they currently have existing access roads.

10. What is the slope (horizontal/vertical) of the cut and fill areas proposed to be? What methods will be used to prevent erosion until the revegetation is established?

The maximum slope of any cut and fill area is 6:1. The methods to prevent erosion are provided by the silt fence

11. Are you planning any berms?

Yes	No X	If yes, how tall is the berm at its highest?	

12. If your property slopes and you are leveling a pad for a building, are retaining walls going to be required? If so, how high will the walls be and what is their construction (i.e. rockery, concrete, timber, manufactured block)?

A proposed rockery wall located at the southern boundary is a maximum of 6 ft tall.

13. What are you proposing for visual mitigation of the work?



14. Will the grading proposed require removal of any trees? If so, what species, how many and of what size?

No, the grading is intended to increase the survivability of trees planted on the property.

15. What type of revegetation seed mix are you planning to use and how many pounds per acre do you intend to broadcast? Will you use mulch and, if so, what type?

The seed mix is call dryland wildflower mix by Comstock Feed. The recommended density is 1 lb per 3,000 sq foot.

16. How are you providing temporary irrigation to the disturbed area?

Water truck and hose line.

- 17. Have you reviewed the revegetation plan with the Washoe Storey Conservation District? If yes, have you incorporated their suggestions?
- 18. Are there any restrictive covenants, recorded conditions, or deed restrictions (CC&Rs) that may prohibit the requested grading?

Yes	NoX	If yes, please attach a copy.

### Special Use Permit Application for Stables Supplemental Information

(All required information may be separately attached)

1. What is the maximum number of horses to be boarded, both within stables and pastured?

Landscaping to be added throughout the project and continued into post project timelines.

2. What is the maximum number of horses owned/maintained by the owner/operator of the project, both within stables and pastured?

N/A

3. List any ancillary or additional uses proposed (e.g., tack and saddle sales, feed sales, veterinary services, etc.). Only those items that are requested may be permitted.

N/A

4. If additional activities are proposed, including training, events, competition, trail rides, fox hunts, breaking, roping, etc., only those items that are requested may be permitted. Clearly describe the number of each of the above activities which may occur, how many times per year and the number of expected participants for each activity.

N/A

5. What currently developed portions of the property or existing structures are going to be used with this permit?

N/A

6. To what uses (e.g., restrooms, offices, managers living quarters, stable area, feed storage, etc.) will the barn be put and will the entire structure be allocated to those uses? (Provide floor plans with dimensions).

N/A

7. Where are the living quarters for the operators of the stables and where will employees reside?

N/A

8. How many improved parking spaces, both on-site and off-site, are available or will be provided? (Please indicate on site plan.) Have you provided for horse trailer turnarounds?

N/A

9. What are the planned hours of operation?

N/A

10. What improvements (e.g. new structures including the square footage, roadway/driveway improvements, utilities, sanitation, water supply, drainage, parking, signs, etc.) will have to be constructed or installed and what is the projected time frame for the completion of each?

N/A

11. What is the intended phasing schedule for the construction and completion of the project?

N/A

12. What physical characteristics of your location and/or premises are especially suited to deal with the impacts and the intensity of your proposed use?

Ease of access to the site from the highway, natural drainage paths, site shape and orientation, benefit to neighboring properties.

13. What are the anticipated beneficial aspects or affects your project will have on adjacent properties and the community?

N/A

14. What are the adverse impacts upon the surrounding community (including traffic, noise, odors, dust, groundwater contamination, flies, rats, mice, etc.) and what will you do to minimize the anticipated negative impacts or effects your project will have on adjacent properties?

No, the grading is intended to increase the survivability of trees planted on the property.

15. Please describe operational parameters and/or voluntary conditions of approval to be imposed on the administrative permit to address community impacts.

The seed mix is call dryland wildflower mix by Comstock Feed. The recommended density is 1 lb per 3,000 sq foot.

16. What types of landscaping (e.g. shrubs, trees, fencing, painting scheme, etc.) are proposed? (Please indicate location on site plan.)

N/A

17. What type of signs and lighting will be provided? On a separate sheet, show a depiction (height, width, construction materials, colors, illumination methods, lighting intensity, base landscaping, etc.) of each sign and the typical lighting standards. (Please indicate location of signs and lights on site plan.)

N/A			

18. Are there any restrictive covenants, recorded conditions, or deed restrictions (CC&Rs) that apply to the area subject to the administrative permit request? (If so, please attach a copy.)

Yes	No No
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19. Community Sewer

Yes	No No

20. Community Water

No
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# Reno Tahoe Geo Associates, Inc.

Sheet of II

 PROJECT
 I 90 US HIGHWAY 395 S
 PROJECT NO.
 2 | 100.002

 SUBJECT
 ROCKERY WALL DESIGN
 BY
 J. ARCHULETA
 DATE
 1 2/6/202 I

 CALCULATION PACKAGE
 REVIEWED BY
 J. PEASE
 DATE
 1 2/6/202 I

#### PURPOSE

This package includes local and stability calculations and supporting data (strength data, loading types and data, etc).

#### SOIL PROPERTIES AND LOADS

Native soils are assumed to be silty gravelly sand to sandy gravel with shallow bedrock. Assumed and calculated properties include:

Soil Unit Weight (¥)		128 pcf
Friction Angle (Ø)		35 degrees
Active Earth Coefficient (Ka)	=	0.29
Pseudo-static Active Earth Coefficient (Kae)		0.93
Cohesion (c)		0 pcf

#### LOADS

Peak Ground Acceleration (use 50% for calculations) = 0.946 g

#### RESULTS

Local stability calculations show that the walls are stable with regard to sliding, overturning, and bearing capacity for static and seismic conditions per FHWA-CFL/TD-O6-OO6, November 2006, *Rockery Design and Construction Guidelines.* 

Wedge analysis was used to determine active earth coefficients Ka and Kae for all soils.

Global stability shows that the walls have the minimum factor of safety of at least 2.15 against static stability and the minimum factor of safety of at least 1.04 against seismic stability.

#### ATTACHMENTS:

Pages	Items
	Summary
2 - 3	Local Wall Stability
4 - 5	Global Wall Stability
6 - 7	Active Pressure Coefficients
8 - 10	Seismic Parameters (ASCE 7 Hazards Report)
	WI.O Rockery Wall Details



<sup>3</sup> Approved ( 07/12/2022

#### **ROCKERY WALL CALCULATIONS**

Sheet 2 of 11

JECT :	100 118 205		DV.							
	190 US 395		BY:		DATE:	11/23/21				
JECT NO:	21100.002	(	CHECKED BY		DATE:	11/24/2021				
ATION:	Washoe Valley			Spreadsheet re	viewed JWP 4/1/2	2015				
:										
INPUT			MAXIMUM EXP	OSED WALL H	EIGHT 4 ft					
•	Vall Height, h (ft)		4	FHWA Design						
	Width, Cw (ft)		3.75			ckfill is vertical. Method				
	Width, Bw (ft)	A	4.75			f backfill behind wall (c				
	dment Depth, De (fi	,		2 1.5 ft minimum on flat, FLH recommends on slopes, soil 18 cover extends downhill at least 6 feet from bottom of wall						
	ackfill Behind Wall, /eight, Gamasoil (pe		128							
	all Soil Friction Ang	,	35	Native soil.						
	Soil Friction Angle		35		nhi for sliding alo	ng base if base soils b	etter			
	Unit Weight, Gamm		140	May use nigher	pril for silding alo	ing base in base solis b	ellei			
	I Contact Friction A	. ,	23	•						
Surcharge			0							
	ve Earth Coefficient	. Ka	0.29							
	atic Active Earth Co		0.93	Based on half o	f the site PGA					
	Seismic Coefficien	•	0.32			be about one-third of the si	te PGA			
Method genera	ally but does not strictly fo	low Rockery Design and	Construction Guidelin	es, 2006,Federal La	nds Highway Division	FHWA-CFL-TD-06-006				
CALCUL										
L1 = 2/3 x (	Bw - Cw), ft				F1 = 0.5 x Ka(or	Kae) x Gamasoil x (h+	de)^2			
L2 = Bw - 0	.5 x Cw, ft				F2 = q x (h+de) :	x Ka(or Kae)				
W2 = Cw x	(Bw - Cw) x (h + De) (h + De) x Gamarocl NING FACTOR OF S	k, lbs			Ea = F1 + F2					
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA	(h + De) x Gamarocl	x, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1*	h/3 + W2*h/3)	Cos(ξr) x (h/3 + [		) x (h/2 + De))				
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY	x, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))] ) / (Ea	h/3 + W2*h/3) x cos(ξr))	Cos(ξr) x (h/3 + [		) x (h/2 + De))				
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan W1L1	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY ( $\phi$ r)) x [W1 + W2 + (H2) plus for seismic, FD W2L2	x, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))] ) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b>	h/3 + W2*h/3) x cos(ξr)) F2)	h/3 + De		) x (h/2 + De)) (h/2 + De)	Batter			
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W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tan) <b>W1L1</b> 281 <b>L1</b> 0.67 <b>W1</b>	(h + De) x Gamarocl <b>NING FACTOR OF S</b> MD=((W1 x L1) + (W2 plus for seismic MD <b>ACTOR OF SAFETY</b> (φr)) x [W1 + W2 + (H plus for seismic, FD <u>W2L2</u> 9056 <u>L2</u> 2.875 <u>W2</u> 3150 <b>FS</b>	x, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))]) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b> 1240 3977 <b>F1 (Static)</b> 668 <b>F1 (Seismic)</b> 2143	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tan) <b>W1L1</b> 281 <b>L1</b> 0.67 <b>W1</b>	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY ( $\varphi$ r)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin( includes +Kh*(W1*</li> <li>Ea x sin(ξr))] ) / (Ea includes +Kh*(F1+</li> <li>Ea x Sin(ξr) x Bw 1240 3977</li> <li>F1 (Static) 668</li> <li>F1 (Seismic) 2143</li> </ul>	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b>	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tan) <b>W1L1</b> 281 <b>L1</b> 0.67 <b>W1</b>	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning	x, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))]) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b> 1240 3977 <b>F1 (Static)</b> 668 <b>F1 (Seismic)</b> 2143	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tan) <b>W1L1</b> 281 <b>L1</b> 0.67 <b>W1</b>	(h + De) x Gamarocl <b>NING FACTOR OF S</b> MD=((W1 x L1) + (W2 plus for seismic MD <b>ACTOR OF SAFETY</b> (φr)) x [W1 + W2 + (H plus for seismic, FD <u>W2L2</u> 9056 <u>L2</u> 2.875 <u>W2</u> 3150 <b>FS</b>	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin( includes +Kh*(W1*</li> <li>Ea x sin(ξr))] ) / (Ea includes +Kh*(F1+</li> <li>Ea x Sin(ξr) x Bw 1240 3977</li> <li>F1 (Static) 668</li> <li>F1 (Seismic) 2143</li> </ul>	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b>	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan) U1 281 L1 0.67 W1 420	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning (Static) 5.2	x, lbs <b>SAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))]) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b> 1240 3977 <b>F1 (Static)</b> 668 <b>F1 (Seismic)</b> 2143 <b>FS Overturning</b> (Seismic) <b>1.21</b>	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615 'Seismic sliding a	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b> <b>(Static)</b> <b>4.4</b>	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding (Seismic) 1.0	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan) W1L1 281 L1 0.67 W1	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning (Static)	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin( includes +Kh*(W1*</li> <li>Ea x sin(ξr))] ) / (Ea includes +Kh*(F1+</li> <li>Ea x Sin(ξr) x Bw 1240</li> <li>3977</li> <li>F1 (Static)</li> <li>668</li> <li>F1 (Seismic)</li> <li>2143</li> </ul> FS Overturning (Seismic)	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615 Seismic sliding a	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b> <b>(Static)</b>	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding (Seismic)	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan) U1 281 L1 0.67 W1 420	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning (Static) 5.2	x, lbs <b>SAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))]) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b> 1240 3977 <b>F1 (Static)</b> 668 <b>F1 (Seismic)</b> 2143 <b>FS Overturning</b> (Seismic) <b>1.21</b>	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 x	h/3 + De 3.3 Frs 3087 Fds 615 Seismic sliding a	De) + F2 x Cos(ξr) <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b> <b>(Static)</b> <b>4.4</b>	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding (Seismic) 1.0	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan) U1 281 L1 0.67 W1 420	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning (Static) 5.2	x, lbs <b>SAFETY</b> 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))]) / (Ea includes +Kh*(F1+ <b>Ea x Sin(ξr) x Bw</b> 1240 3977 <b>F1 (Static)</b> 668 <b>F1 (Seismic)</b> 2143 <b>FS Overturning</b> (Seismic) <b>1.21</b>	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 3.3 Frs 3087 Fds 615 Seismic sliding a	De) + F2 x Cos(ξr) 0 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b> <b>(Static)</b> <b>4.4</b> 1.5	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding (Seismic) 1.0	4/1 Ea (Statio 668 Ea (Seism 2143			
W2 = Cw x OVERTURI FSo = MR/I SLIDING FA FSs = ((tan) W1L1 281 L1 0.67 W1 420 MIN FS WEIGHT	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H2 plus for seismic, FD W2L2 9056 L2 2.875 W2 3150 FS Overturning (Static) 5.2 1.5	x, lbs SAFETY 2 x L2) + (Ea x Sin( includes +Kh*(W1* Ea x sin(ξr))] ) / (Ea includes +Kh*(F1+ Ea x Sin(ξr) x Bw 1240 3977 F1 (Static) 668 F1 (Seismic) 2143 FS Overturning (Seismic) 1.21 1.1 BEARING	h/3 + W2*h/3) x cos(ξr)) F2) F1 x Cos(ξr) 615 1972 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 3.3 Frs 3087 Fds 615 Seismic sliding a MIN FS ACITY	De) + F2 x Cos(ξr) 0 0 <b>MR (Static)</b> 10578 <b>MD (Static)</b> 2050 and overturning a <b>FS Sliding</b> <b>(Static)</b> <b>4.4</b> 1.5	(h/2 + De) 4.0 MR (Seismic) 13314 MD (Seismic) 10985 ssume no F2 surcharg FS Sliding (Seismic) 1.0 1	4/1 Ea (Statio 668 Ea (Seism 2143			

PASSWORD = ROCKERY

Reno Tahoe Geo Associates P.O. Box 18449 Reno, NV 89511 Tel: 775-853 9100

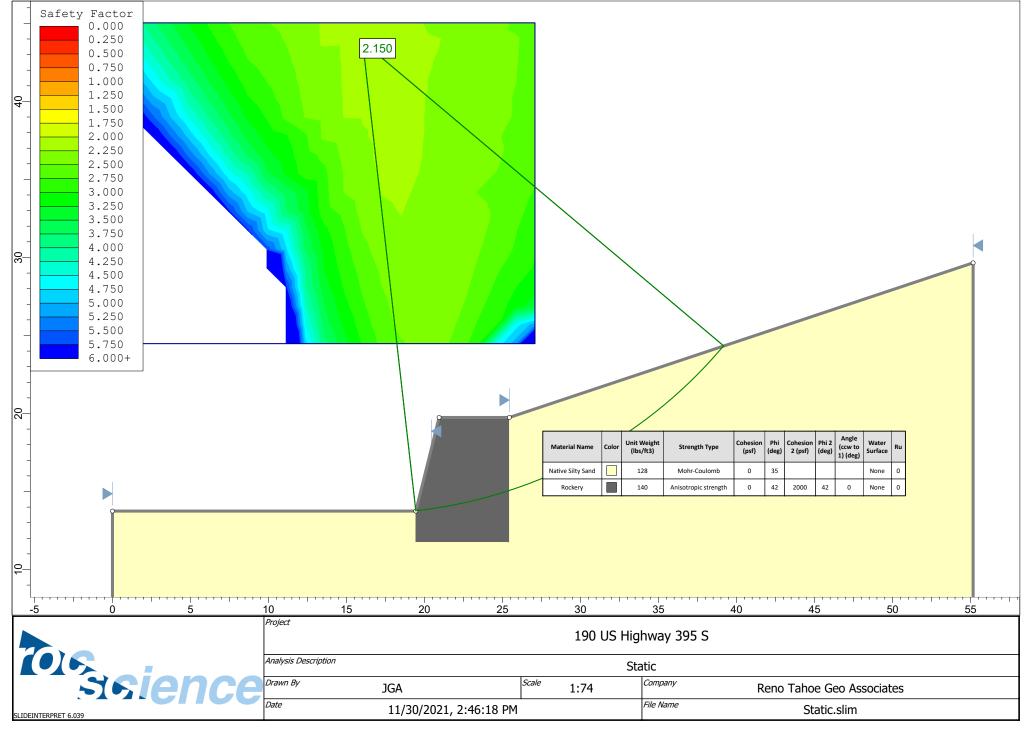
#### **ROCKERY WALL CALCULATIONS**

Sheet 3 of 11

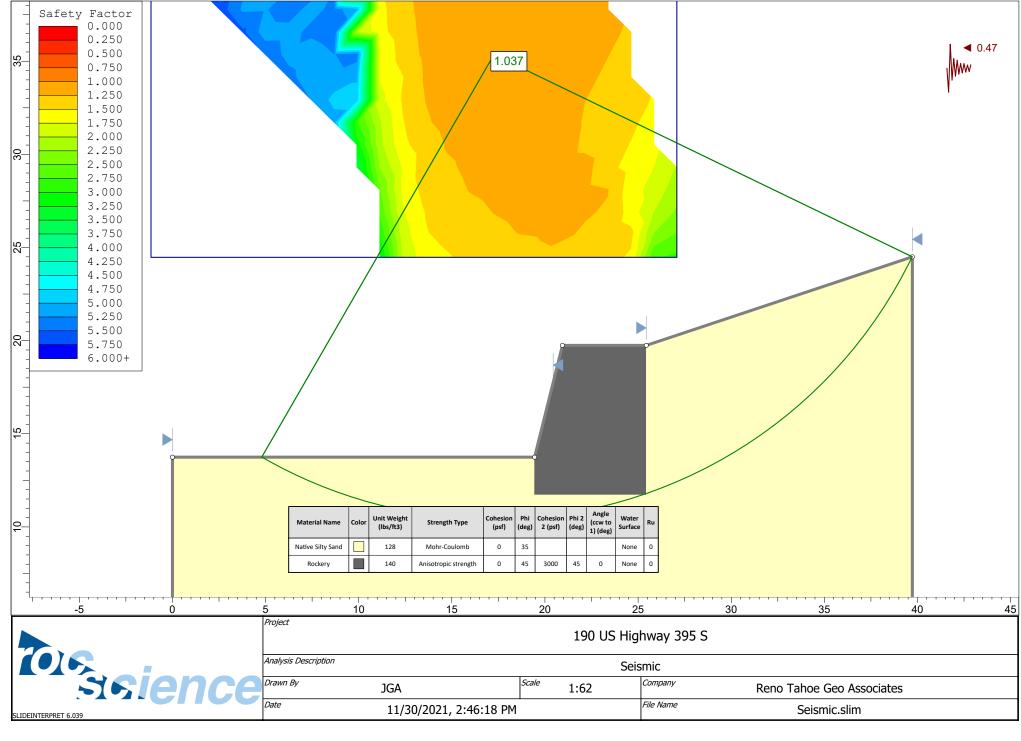
OJE	CT:	190 US 395		BY:	JGA	DATE:	11/23/21				
OJE	CT NO:	21100.002	C	HECKED BY	JWP	DATE:	11/24/202	1			
CA	FION:	Washoe Valley			Spreadsheet re	viewed JWP 4/1/2	2015				
es:											
	INPUT			MAXIMUM EXP	OSED WALL H	EIGHT 6 ft					
	Exposed W	/all Height, h (ft)		6 FHWA Design Comments							
	Wall Crest Width, Cw (ft)			4.5	Method assume	es back of wall/ba	ckfill is vertical. Method	d does			
		Width, Bw (ft)		6			f backfill behind wall (c				
	Wall Embedment Depth, De (ft) Angle of Backfill Behind Wall, βr (deg)			2 1.5 ft minimum on flat, FLH recommends on slopes, soil							
	-			18 cover extends downhill at least 6 feet from bottom of wall							
		eight, Gamasoil (po Il Soil Friction Ang	,	128 35	Native soil.						
		Soil Friction Angle				phi for sliding alc	ong base if base soils b	etter			
		Unit Weight, Gamm		140	may use mighter	printer enang are		ottor			
		I Contact Friction A	. ,	23							
	Surcharge,	q (lbf/ft)		0							
		e Earth Coefficient		0.29							
		tic Active Earth Co	,	0.93	Based on half c						
		Seismic Coefficien	•		0		be about one-third of the si	te PGA			
	•	ally but does not strictly fo	IOW ROCKERY Design and	onstruction Guidelin	es, 2006,Federal La	nas Highway Division	FHWA-CFL-1D-06-006				
	<b>CALCUL</b> L1 = 2/3 x (					F1 = 0.5 x Ka(or	- Kae) x Gamasoil x (h+	-de)^2			
						,	,	40) 2			
	L2 = Bw - 0	.5 x CW, π		F2 = q x (h+de) x Ka(or Kae)							
				Fa = F1 + F2							
	W1 = 0.5 x	(Bw - Cw) x (h + De)	x Gamarock, lbs			Ea = F1 + F2					
		(Bw - Cw) x (h + De) (h + De) x Gamarocl				Ea = F1 + F2					
	W2 = Cw x OVERTURI FSo = MR/N SLIDING FA	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (f	ς, lbs SAFETY 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x	h/3 + W2*h/3) $a \cos(\xi r))$	Cos(ξr) x (h/3 + [		) x (h/2 + De))				
	W2 = Cw x OVERTURI FSo = MR/N SLIDING FA FSs = ((tan	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (f plus for seismic, FD	ς, lbs SAFETY 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F	/3 + W2*h/3) cos(ξr)) 2)		De) + F2 x Cos(ξr		Batter			
	W2 = Cw x OVERTURI FSo = MR/N SLIDING FA	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (f	ς, lbs SAFETY 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x	h/3 + W2*h/3) $a \cos(\xi r))$	Cos(ξr) x (h/3 + [ h/3 + De 4.0		) x (h/2 + De)) (h/2 + De) 5.0	Batter 4/1			
	W2 = Cw x OVERTURI FSo = MR/N SLIDING FA FSs = ((tan W1L1	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (I plus for seismic, FD W2L2	c, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F <b>Ea x Sin(ξr) x Bw</b>	i/3 + W2*h/3) cos(ξr)) 2) <b>F1 x Cos(ξr)</b>	h/3 + De	De) + F2 x Cos(ξr F2 x Cos(ξr)	(h/2 + De)				
	W2 = Cw x OVERTURI FSo = MR/N SLIDING FA FSs = ((tan W1L1	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (I plus for seismic, FD W2L2 18900 L2	c, lbs <b>CAFETY</b> 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F Ea x Sin(ξr) x Bw 2785	/3 + W2*h/3) 2) F1 x Cos(ξr) 1093	h/3 + De	De) + F2 x Cos(ξr F2 x Cos(ξr) 0	(h/2 + De)				
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (I plus for seismic, FD W2L2 18900 L2 3.75	<ul> <li>k, Ibs</li> <li><b>CAFETY</b></li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h)</li> <li>Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F)</li> <li>Ea x Sin(ξr) x Bw 2785</li> <li>8930</li> <li>F1 (Static)</li> <li>1188</li> </ul>	/3 + W2*h/3) 2 cos(ξr)) 2 <b>F1 x Cos(ξr)</b> 1093 3506 <b>F2 (Static)</b> 0	h/3 + De 4.0 Frs 4704	De) + F2 x Cos(ξr <b>F2 x Cos(ξr)</b> 0 0 <b>MR (Static)</b> 22529	(h/2 + De) 5.0 MR (Seismic) 28675	4/1 Ea (Static 1188			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (I plus for seismic, FD W2L2 18900 L2 3.75 W2	<ul> <li>k, Ibs</li> <li><b>SAFETY</b></li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F Ea x Sin(ξr) x Bw 2785 8930 F1 (Static) 1188 F1 (Seismic)</li> </ul>	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic)	h/3 + De 4.0 Frs 4704 Fds	De) + F2 x Cos(ξr <b>F2 x Cos(ξr)</b> 0 <b>MR (Static)</b> 22529 <b>MD (Static)</b>	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic)	4/1 Ea (Static 1188 Ea (Seismi			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (I plus for seismic, FD W2L2 18900 L2 3.75	<ul> <li>k, Ibs</li> <li><b>CAFETY</b></li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h)</li> <li>Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F)</li> <li>Ea x Sin(ξr) x Bw 2785</li> <li>8930</li> <li>F1 (Static)</li> <li>1188</li> </ul>	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarock NING FACTOR OF S $MD=((W1 \times L1) + (W2))$ plus for seismic MD ACTOR OF SAFETY ( $\phi$ r)) x [W1 + W2 + (H2)) plus for seismic, FD W2L2 18900 L2 3.75 W2 5040	<ul> <li>k, Ibs</li> <li><b>SAFETY</b></li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F Ea x Sin(ξr) x Bw 2785 8930 F1 (Static) 1188 F1 (Seismic)</li> </ul>	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic)	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS	x, lbs <b>SAFETY</b> 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F <b>Ea x Sin(ξr) x Bw</b> 2785 8930 <b>F1 (Static)</b> 1188 <b>F1 (Seismic)</b> 3809	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 ssume no F2 surcharg	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W) plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (f plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h)</li> <li>Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F)</li> <li>Ea x Sin(ξr) x Bw</li> <li>2785</li> <li>8930</li> <li>F1 (Static)</li> <li>1188</li> <li>F1 (Seismic)</li> <li>3809</li> </ul> FS Overturning	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 Issume no F2 surcharg	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS	x, lbs <b>SAFETY</b> 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F <b>Ea x Sin(ξr) x Bw</b> 2785 8930 <b>F1 (Static)</b> 1188 <b>F1 (Seismic)</b> 3809	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 ssume no F2 surcharg	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W) plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (f plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h)</li> <li>Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F)</li> <li>Ea x Sin(ξr) x Bw</li> <li>2785</li> <li>8930</li> <li>F1 (Static)</li> <li>1188</li> <li>F1 (Seismic)</li> <li>3809</li> </ul> FS Overturning	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 Issume no F2 surcharg	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> / FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b> 840	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W) plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning (Static) 5.2	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F Ea x Sin(ξr) x Bw 2785 8930</li> <li>F1 (Static) 1188</li> <li>F1 (Seismic) 3809</li> </ul> FS Overturning (Seismic) 1.25	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093 Seismic sliding	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding (Static) 4.1	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 Issume no F2 surcharg FS Sliding (Seismic) 1.0	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b>	(h + De) x Gamarock NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning (Static)	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h)</li> <li>Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F)</li> <li>Ea x Sin(ξr) x Bw 2785 8930</li> <li>F1 (Static) 1188</li> <li>F1 (Seismic) 3809</li> <li>FS Overturning (Seismic)</li> </ul>	/3 + W2*h/3) cos(ξr)) 2) F1 x Cos(ξr) 1093 3506 F2 (Static) 0 F2 (Seismic) 0 *	h/3 + De 4.0 Frs 4704 Fds 1093 Seismic sliding	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding (Static)	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 Issume no F2 surcharg FS Sliding (Seismic)	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> / FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b> 840	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W2 plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning (Static) 5.2 1.5	<ul> <li>k, Ibs</li> <li>SAFETY</li> <li>2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F Ea x Sin(ξr) x Bw 2785 8930</li> <li>F1 (Static) 1188</li> <li>F1 (Seismic) 3809</li> </ul> FS Overturning (Seismic) 1.25	<pre>//3 + W2*h/3) cos({r)) 2) F1 x Cos({r) 1093 3506 F2 (Static) 0 F2 (Static) 0 F2 (Seismic) 0 * BEARING CAP</pre>	h/3 + De 4.0 Frs 4704 Fds 1093 Seismic sliding MIN FS ACITY	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding (Static) 4.1 1.5	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 issume no F2 surcharg FS Sliding (Seismic) 1.0 1	4/1 Ea (Static 1188 Ea (Seismi 3809			
	W2 = Cw x <b>OVERTURI</b> FSo = MR/N <b>SLIDING F</b> A FSs = ((tank <b>W1L1</b> 844 <b>L1</b> 1.005 <b>W1</b> 840 <b>MIN FS</b>	(h + De) x Gamarocl NING FACTOR OF S MD=((W1 x L1) + (W) plus for seismic MD ACTOR OF SAFETY (φr)) x [W1 + W2 + (H plus for seismic, FD W2L2 18900 L2 3.75 W2 5040 FS Overturning (Static) 5.2	c, Ibs <b>SAFETY</b> 2 x L2) + (Ea x Sin(ξ includes +Kh*(W1*h Ea x sin(ξr))] ) / (Ea x includes +Kh*(F1+F <b>Ea x Sin(ξr) x Bw</b> 2785 8930 <b>F1 (Static)</b> 1188 <b>F1 (Seismic)</b> 3809 <b>FS Overturning</b> (Seismic) 1.25 1.1	<pre>//3 + W2*h/3) cos({r)) 2) F1 x Cos({r) 1093 3506 F2 (Static) 0 F2 (Static) 0 F2 (Seismic) 0 * BEARING CAP</pre>	h/3 + De 4.0 Frs 4704 Fds 1093 Seismic sliding	De) + F2 x Cos(ξr) 0 0 MR (Static) 22529 MD (Static) 4374 and overturning a FS Sliding (Static) 4.1 1.5	(h/2 + De) 5.0 MR (Seismic) 28675 MD (Seismic) 23022 Issume no F2 surcharg FS Sliding (Seismic) 1.0	4/1 Ea (Static 1188 Ea (Seismi 3809			

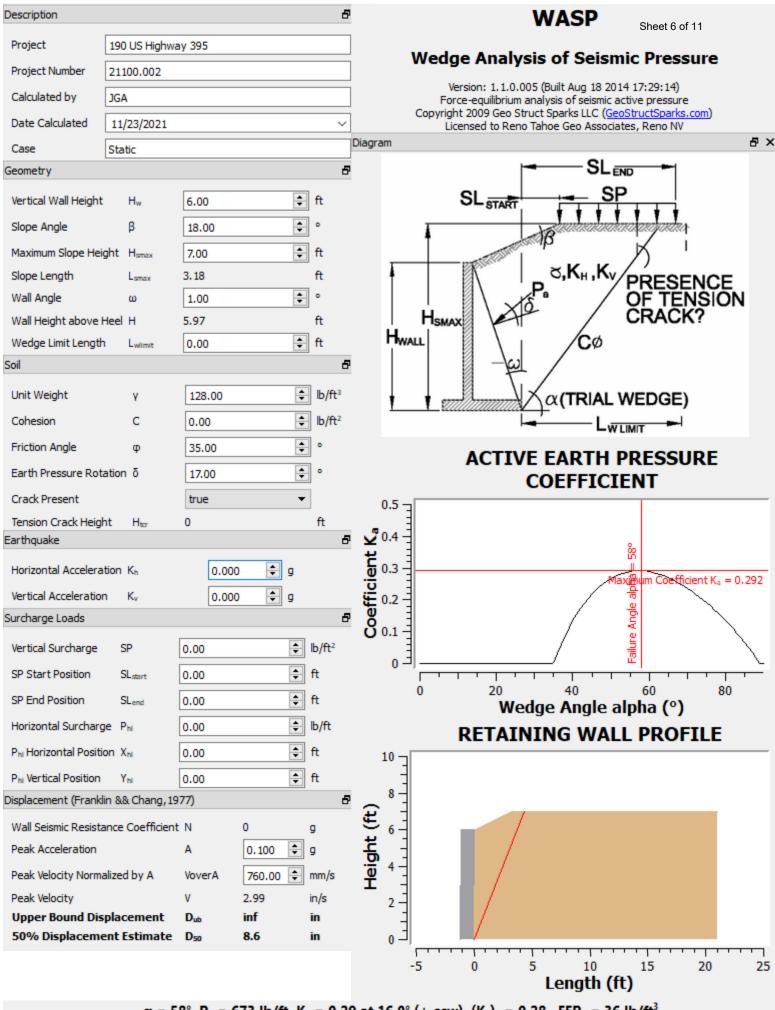
PASSWORD = ROCKERY

Reno Tahoe Geo Associates P.O. Box 18449 Reno, NV 89511 Tel: 775-853 9100

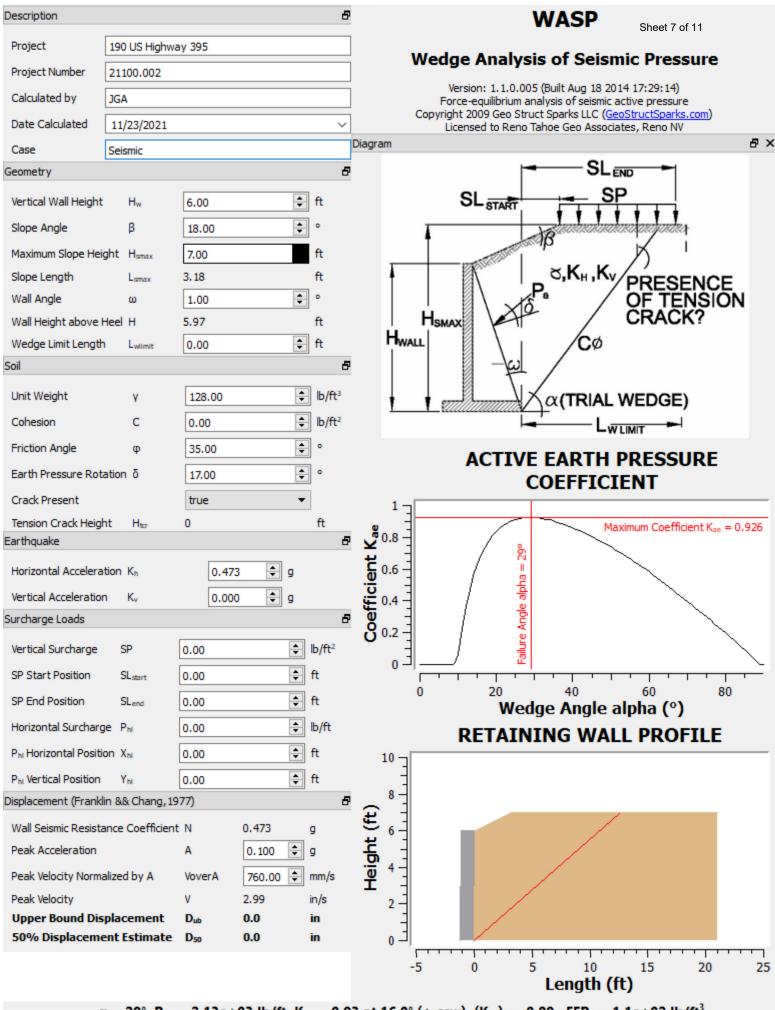








α = 58°, P<sub>a</sub> = 673 lb/ft, K<sub>a</sub> = 0.29 at 16.0° (+ ccw), (K<sub>a</sub>)<sub>h</sub> = 0.28 , EFP<sub>h</sub> = 36 lb/ft<sup>3</sup>



 $\alpha = 29^{\circ}$ ,  $P_{ae} = 2.13e+03 \text{ lb/ft}$ ,  $K_{ae} = 0.93 \text{ at } 16.0^{\circ} (+ \text{ ccw})$ ,  $(K_{ae})_{h} = 0.89$ , EFP<sub>h</sub> = 1.1e+02 lb/ft<sup>3</sup>



Location

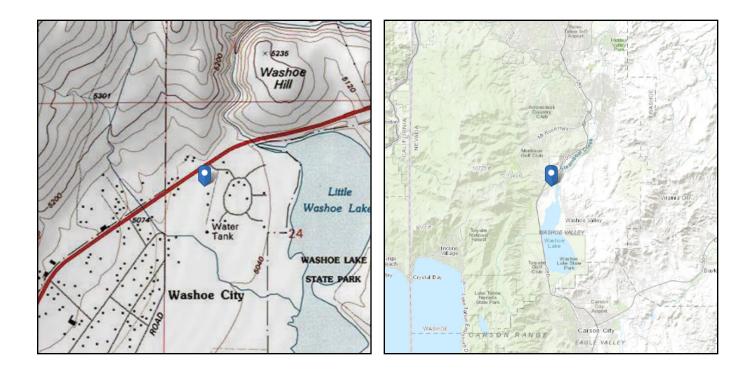
## ASCE 7 Hazards Report

Standard:ASCE/SEI 7-16Risk Category:IIISoil Class:D - Default (see<br/>Section 11.4.3)

 Elevation:
 5060.75 ft (NAVD 88)

 Latitude:
 39.327005

 Longitude:
 -119.805208





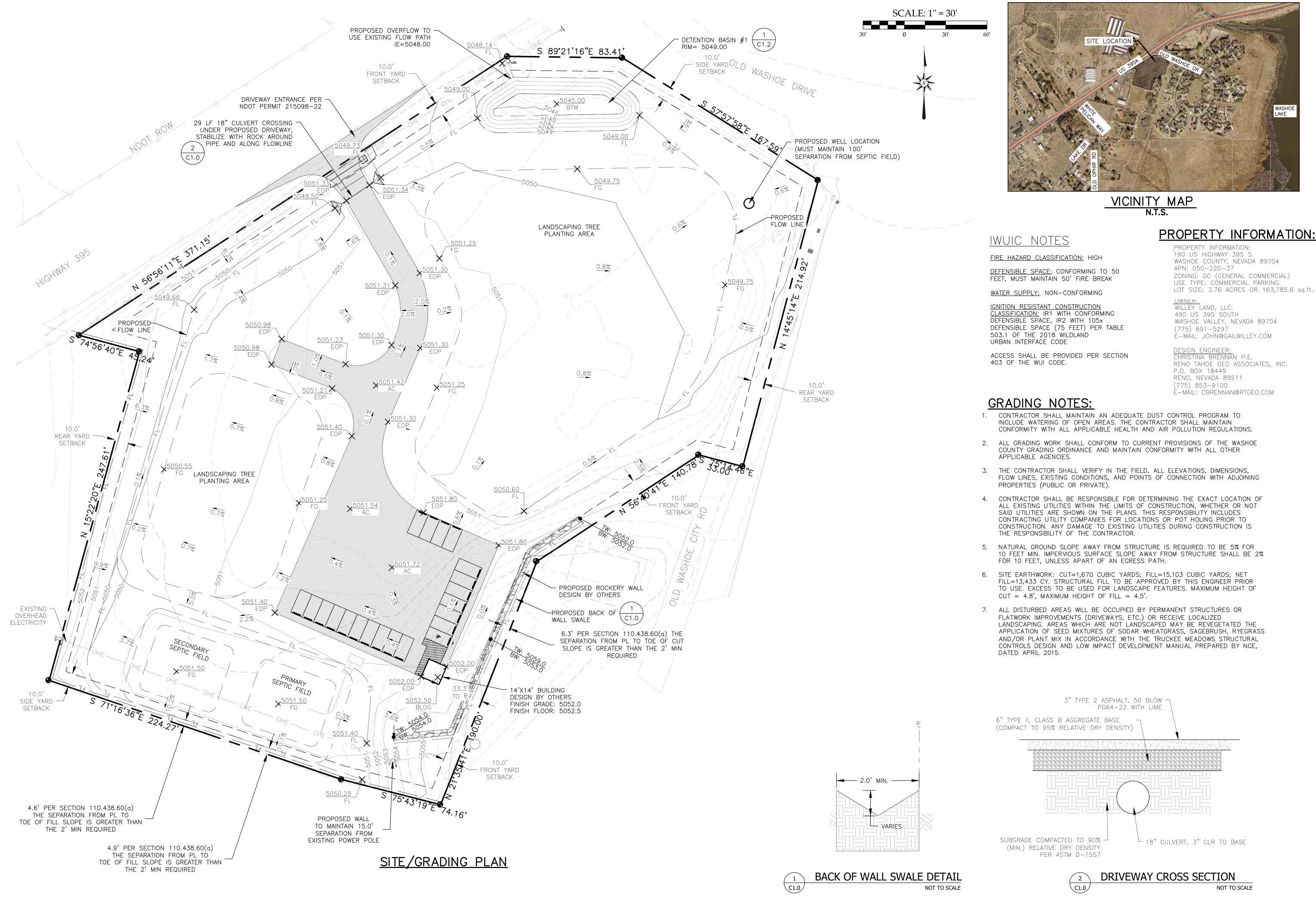
Site Soil Class: Results:	D - Default (see Section 11.4.3)						
S <sub>s</sub> :	2.19	S <sub>D1</sub> :	N/A				
S <sub>1</sub> :	0.77	T <sub>L</sub> :	6				
F <sub>a</sub> :	1.2	PGA :	0.946				
F <sub>v</sub> :	N/A	PGA M:	1.135				
S <sub>MS</sub> :	2.628	F <sub>PGA</sub> :	1.2				
S <sub>M1</sub> :	N/A	l <sub>e</sub> :	1.25				
S <sub>DS</sub> :	1.752	C <sub>v</sub> :	1.5				
Ground motion hazard and	lysis may be required.	See ASCE/SEI 7-16 S	ection 11.4.8.				
Data Accessed:	Tue Nov 23 2	021					
Date Source:	<u>USGS Seismi</u>	<u>c Design Maps</u>					



The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.



CONFORMITY WITH ALL APPLICABLE HEALTH AND AIR POLLUTION REGULATIONS.

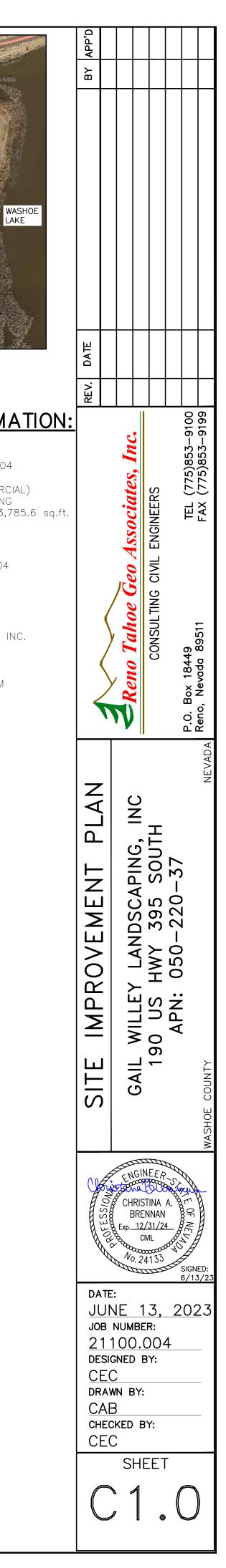
FLOW LINES, EXISTING CONDITIONS, AND POINTS OF CONNECTION WITH ADJOINING

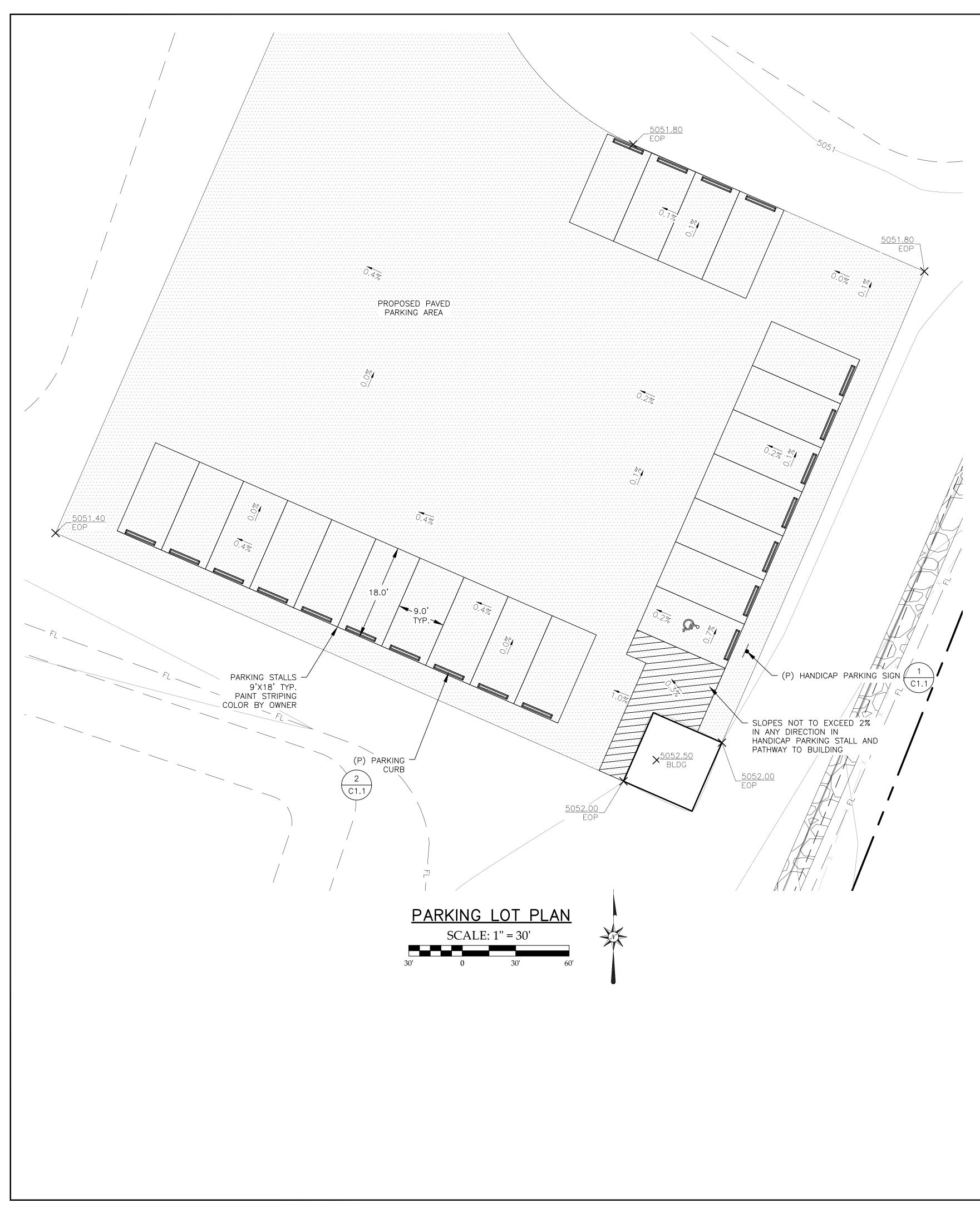
ALL EXISTING UTILITIES WITHIN THE LIMITS OF CONSTRUCTION, WHETHER OR NOT CONTRACTING UTILITY COMPANIES FOR LOCATIONS OR POT HOLING PRIOR TO CONSTRUCTION. ANY DAMAGE TO EXISTING UTILITIES DURING CONSTRUCTION IS

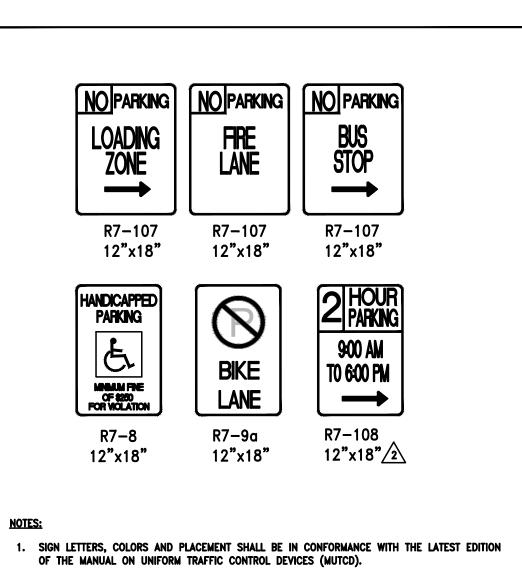
NATURAL GROUND SLOPE AWAY FROM STRUCTURE IS REQUIRED TO BE 5% FOR 10 FEET MIN. IMPERVIOUS SURFACE SLOPE AWAY FROM STRUCTURE SHALL BE 2%

FILL=13,433 CY. STRUCTURAL FILL TO BE APPROVED BY THIS ENGINEER PRIOR TO USE. EXCESS TO BE USED FOR LANDSCAPE FEATURES. MAXIMUM HEIGHT OF

LANDSCAPING. AREAS WHICH ARE NOT LANDSCAPED MAY BE REVEGETATED THE APPLICATION OF SEED MIXTURES OF SODAR WHEATGRASS, SAGEBRUSH, RYEGRASS AND/OR PLANT MIX IN ACCORDANCE WITH THE TRUCKEE MEADOWS STRUCTURAL CONTROLS DESIGN AND LOW IMPACT DEVELOPMENT MANUAL PREPARED BY NCE,







A TIME RESTRICTED PARKING SIGNS ARE AVAILABLE IN 30 MINUTE, 1 HOUR, 2 HOUR, AND 5 HOUR INCREMENTS.

3. REFER TO STANDARD DETAIL DRAWING NO. R-415 FOR MOUNTING AND POLE REQUIREMENTS, UNLESS OTHERWISE SPECIFIED.

DRAWING No.

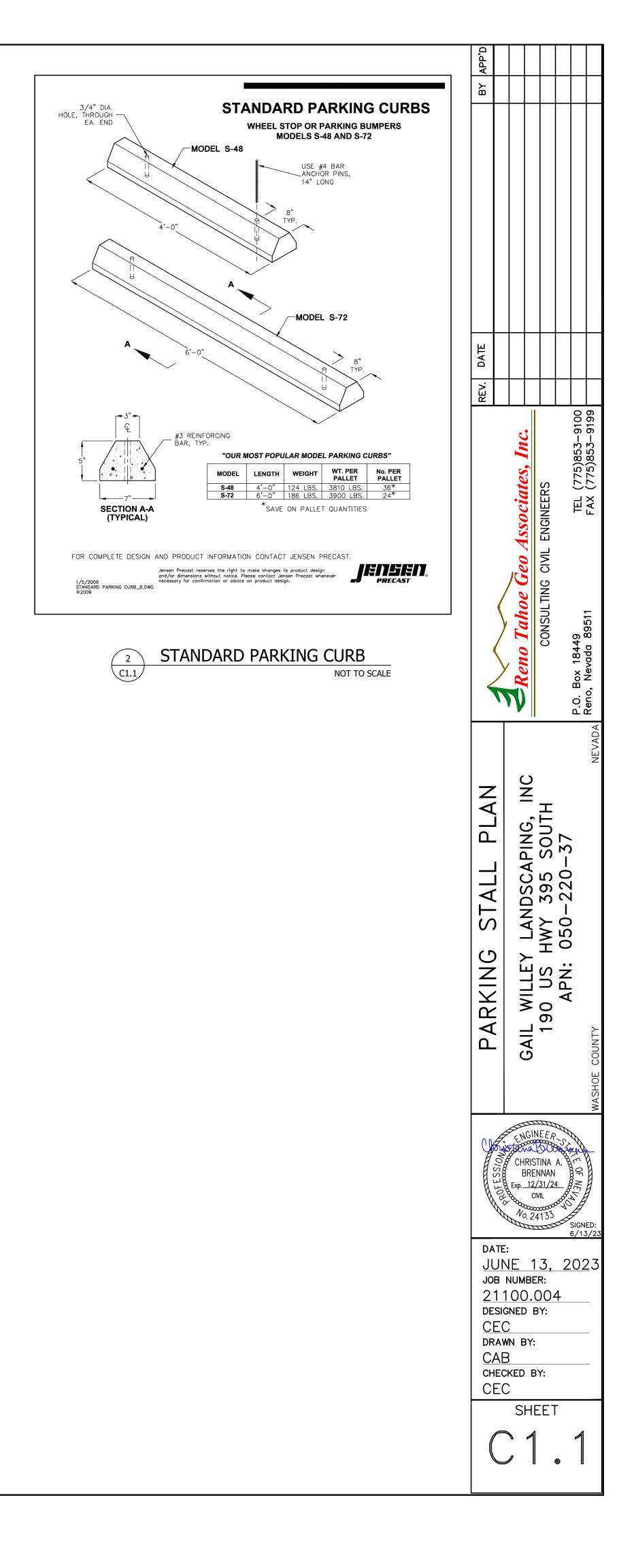
R-414

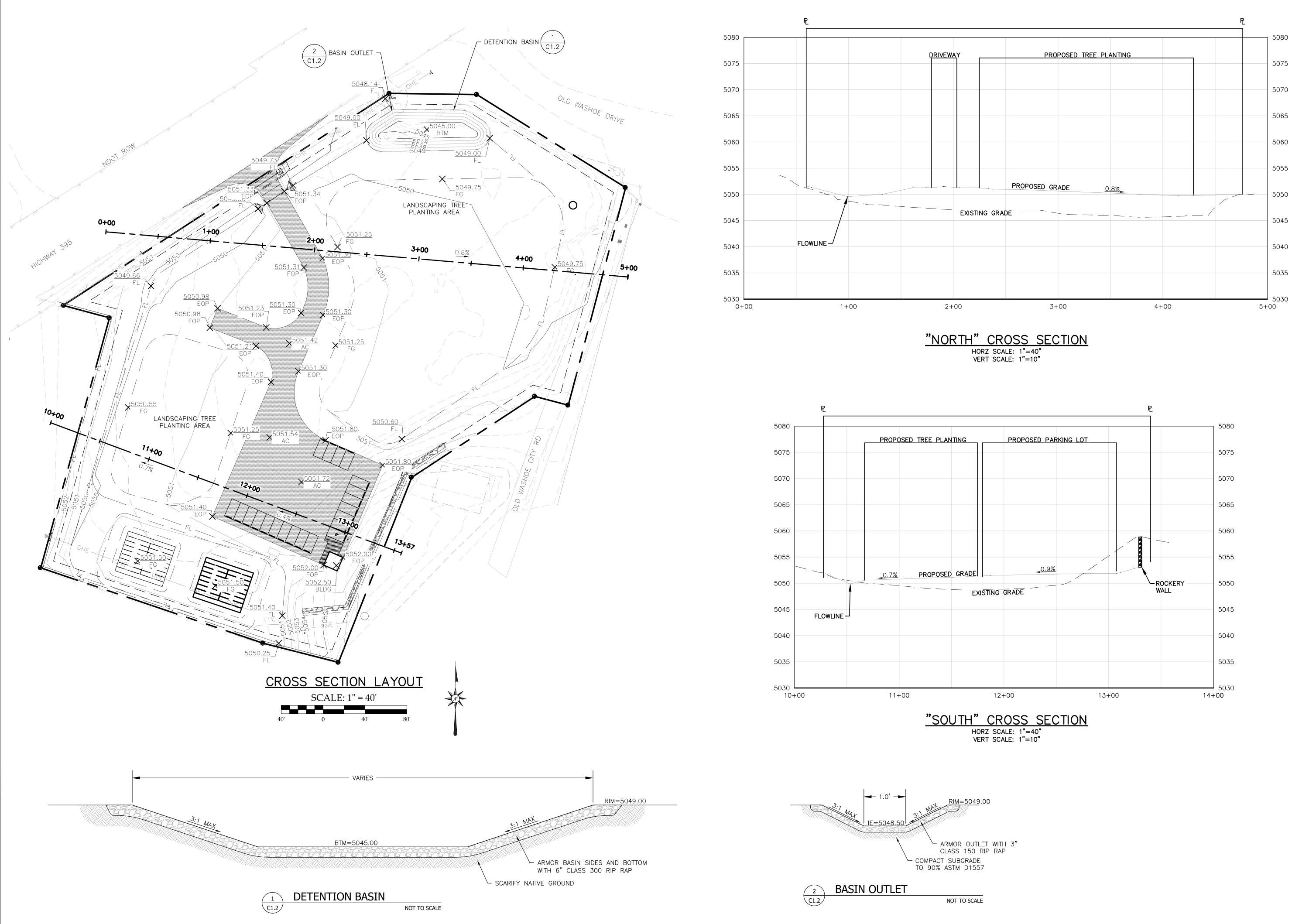
APPROVED BY: JF DATE: 1/2013

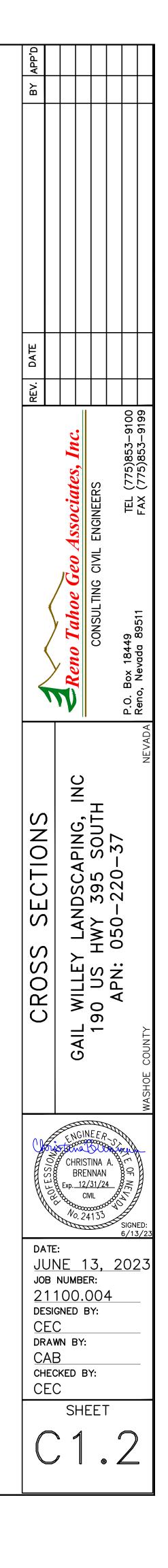
# 1 HANDICAP PARKING SIGN C1.1 NOT TO SCALE

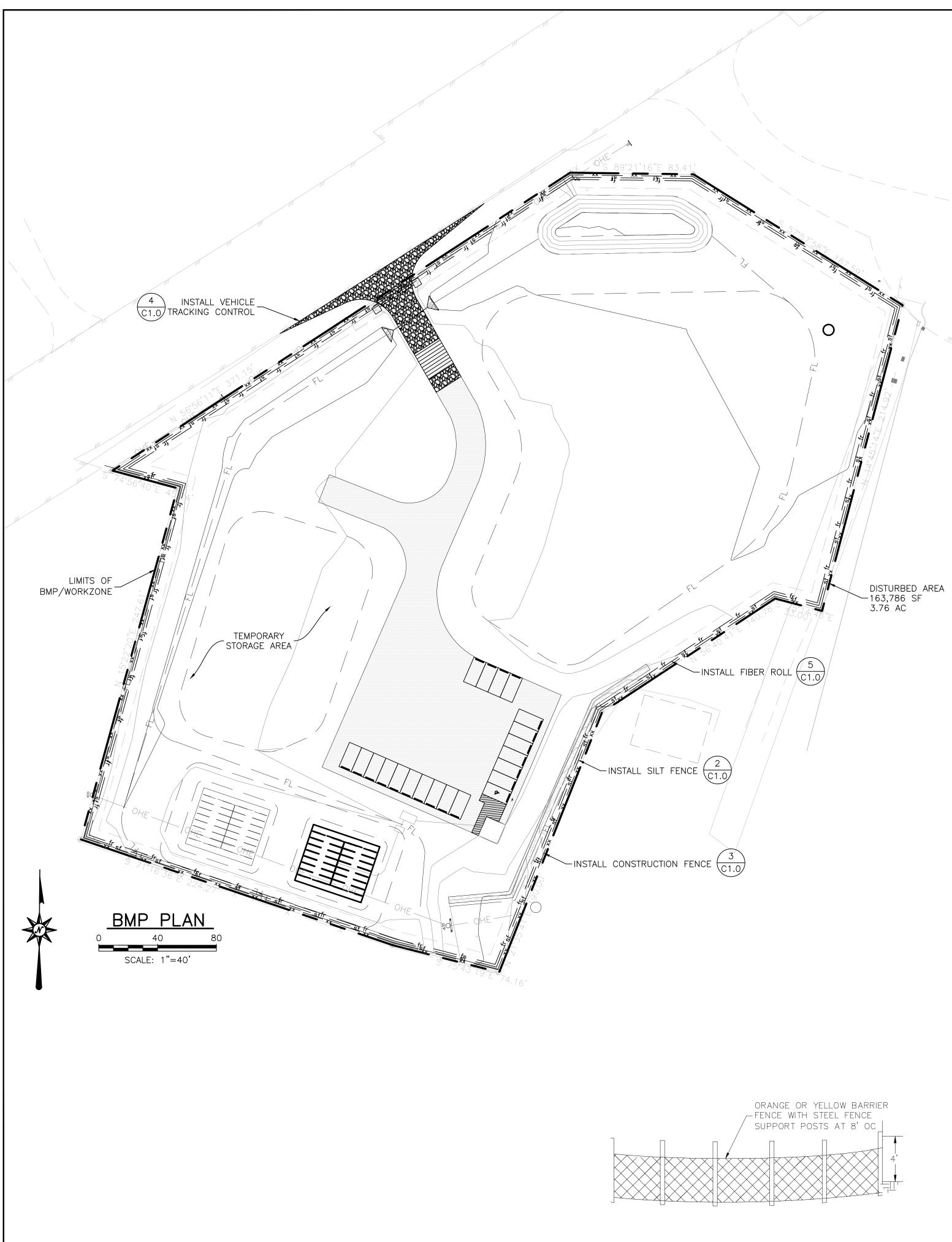
STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION

TRAFFIC PARKING SIGNS



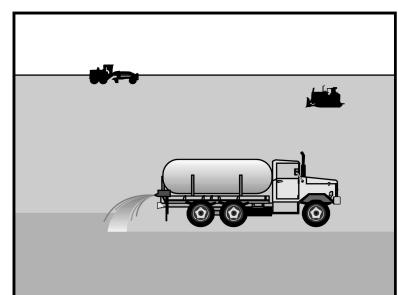






# Wind Erosion and Dust Control

**EC-5** 





Graphics used with permission of Caltrans

Storm water runoff, wind, erosion, and vehicle trackout from construction sites Purpose: can re-disperse sediments to the air by high winds and traffic. Therefore, the purpose of dust control is to minimize these effects.

- All construction sites having exposed soils must perform dust control measures.
- Wind erosion and dust control is important in arid and windy regions.
- Areas with soils with fine particles (silts and clay) are more prone to dust if the surface is disturbed.
- Dust control is a permanent or treatment between but must be adequate upon project completion.
- Dust control methods can help to minimize pollutants in the storm drain system, are generally inexpensive.
- Wind fence (snow fence) are applicable in arid regions where large areas of cleared land are susceptible to blowing sand and dust.

Limitations:

/ 1

Applications:

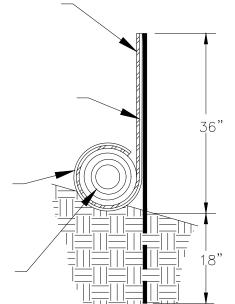
- During construction dust control measures are only temporary and may require reapplication.
- Incorrect usage of chemical stabilizers can have adverse effects on water quality.

Truckee Meadows Regional Storm Water Quality Management Program Construction Site Best Management Practices Handbook, February 2015 Update Section 8 – Erosion Control BMPs

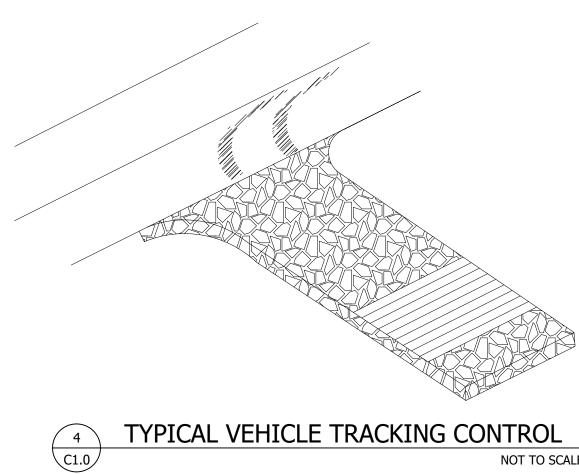
Page 8-11

NOT TO SCALE









TEMPORARY CONSTRUCTION FENCING NOT TO SCALE

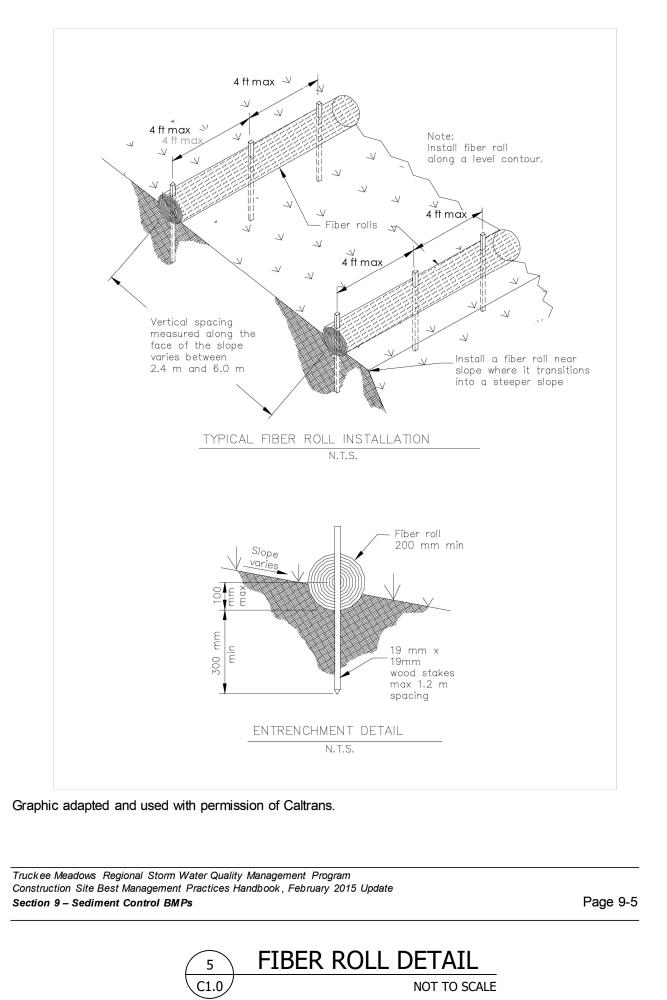
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NOT TO SCALE

Wind Er	osion and Dust Control EC-5	APP'D						
		₽						
	<ul> <li>Discharges from the site can occur if excessive water is applied resulting in runoff.</li> </ul>							
	<ul> <li>Factors such as soil type, temperature, humidity, and wind velocity will impact the effectiveness of the dust control measures.</li> </ul>							
	<ul> <li>Wind fences do not control sediment carried in storm water runoff. Install additional sediment and erosion control measures to capture sediment in runoff (see Section 9).</li> </ul>							
Standards and								
Specifications:	<ul> <li>Follow District Health Department standards and specifications when applying dust control measures at construction sites.</li> </ul>							
	<ul> <li>Wind fences are barriers made of small, evenly spaced wooden slats or fabric. They are erected to reduce wind velocity and to trap blowing sand.</li> </ul>							
	<ul> <li>Erect wind fences perpendicular to the prevailing wind source. Multiple fences may be erected to help prevent wind erosion. Software packages are available to assist with proper design.</li> </ul>							
	<ul> <li>Reduce disturbance of soil crust.</li> </ul>							
	<ul> <li>Other techniques used to control and minimize dust include the application of coarse gravel.</li> </ul>	ATE			_			
	<ul> <li>Magnesium chloride, resins, and lignin sulfonate may be used on roads where revegetation will not occur as these products inhibit plant establishment.</li> </ul>	REV. D.						
0	Application	<u>~</u>				Ĺ		<u>ل</u> م
0	<ul> <li>Moistening road surfaces is an effective dust control method for traffic routes.</li> </ul>			nc.			-91	3-9199
	<ul> <li>This technique is short term and requires constant reapplication especially in windy areas.</li> </ul>			N Sa			്ഥ്	75)853
	<ul> <li>Apply 0.03 - 0.3 gal/yd<sup>2</sup> uniformly to pre-wet the soil surface.</li> </ul>			Associates		RS		(1)
	<ul> <li>Apply 0.125 gal/yd<sup>2</sup> every 20-30 minutes.</li> </ul>					ENGINEERS	ШЦ	FAX
	<ul> <li>Reactivate chemicals in dry climates by rewetting with 0.1 - 0.2 gal/yd<sup>2</sup>.</li> </ul>			S		NGIN		_
	<ul> <li>Avoid ponding.</li> </ul>			N V	•    i			
	<ul> <li>Use a pressure-type distributor or a pipeline equipped with a spray system to evenly distribute water for dust control.</li> </ul>			le o		CIVIL		
	<ul> <li>Provide a positive means to shutoff distribution equipment.</li> </ul>		/		<b>) </b>   {	D N		
	<ul> <li>Provide at least one water truck or hydroseeder to apply water or dust palliative to the construction site.</li> </ul>			ahoe		NSULTING		9511
	If non-notable water is used for dust control all tanks nines and other		y		<b>\$   </b>	ž		95

 If non-potable water is used for dust control, all tanks, pipes, and other conveyances shall be clearly marked with "NON-POTABLE WATER – DO

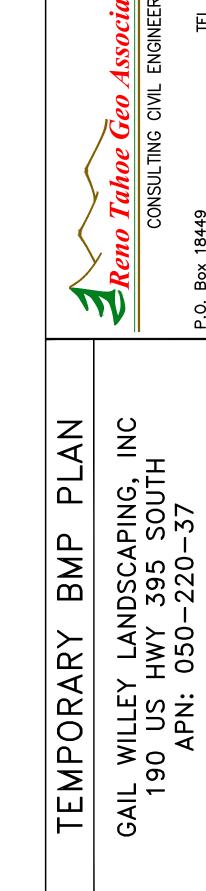
Truckee Meadows Regional Storm Water Quality Management Program Construction Site Best Management Practices Handbook, February 2015 Update Page 8-12 Section 8 – Erosion Control BMPs



NOT TO SCALE

# **Fiber Rolls**

SC-1



FNGINEEA

CHRISTINA BRENNAN

Exp.<u>12/31/24</u> کے CIVIL

<u>JUNE 13, 202</u>3

DATE:

CEC DRAWN BY:

MEM

CEC

JOB NUMBER: 21100.004

DESIGNED BY:

CHECKED BY:

C2.

SHEET

